

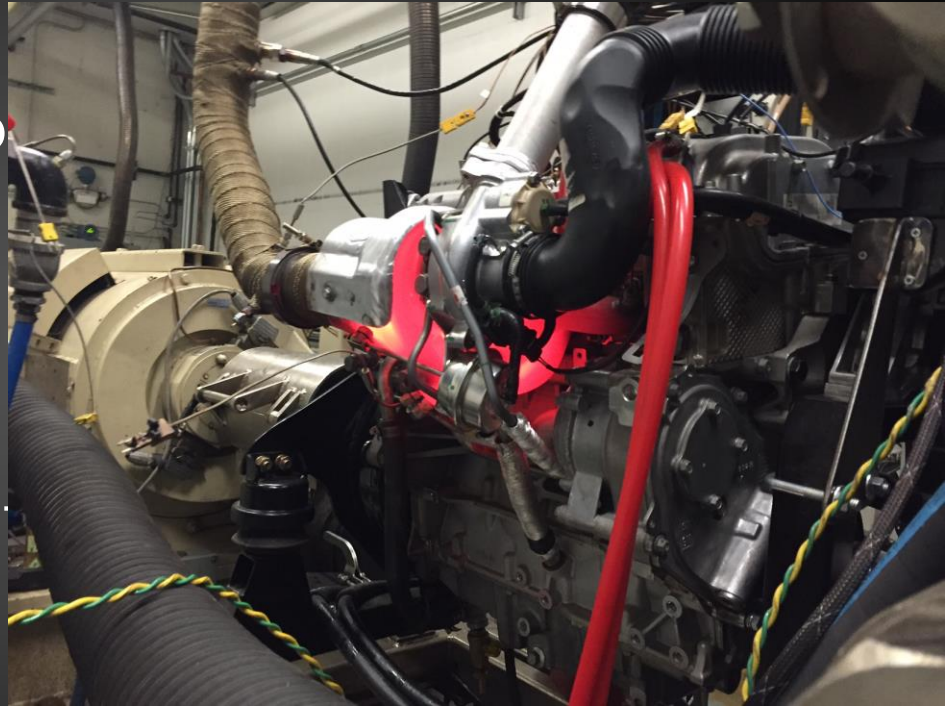
# Lambda 1 High Load Operation via Water Injection

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# Outline

- Motivation
- Experimental Setup
  - Engine Setup
  - Water Injection
  - Controls
- Simulation
- Experimental Results
- Conclusions
- Next Steps



# Motivation



- Avoiding this!
- Enabling the next generation of high efficiency engines

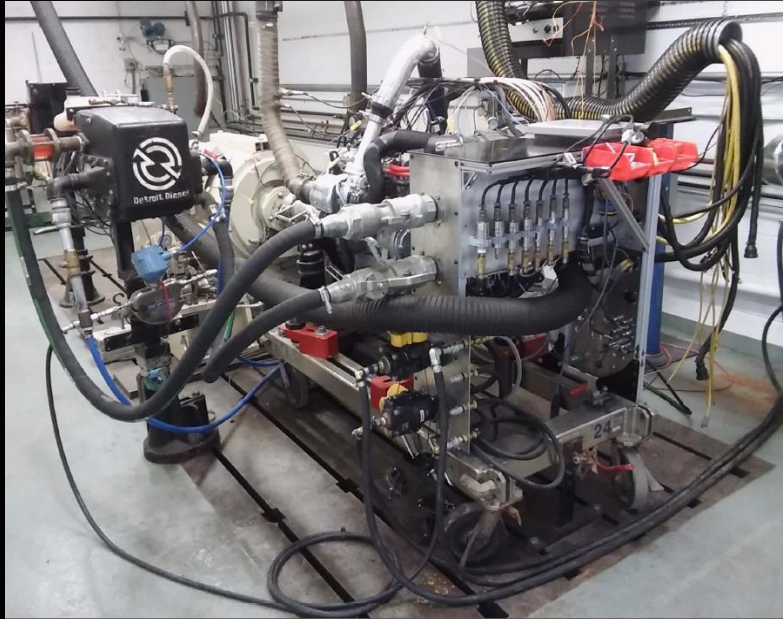
# Motivation

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- Despite increasing popularity, engine “downsizing” does not delivery dramatic real-world fuel economy benefits.
- Downsized engines must be operated at higher loads, often into regions where spark retard and/or over fueling is used to control knock.
- Maximum engine output in SI engines is limited by knock (auto-ignition)
- Mitigation of knock is an enabler for aggressive downsizing AND increased performance

# Experimental Setup

## Baseline Engine



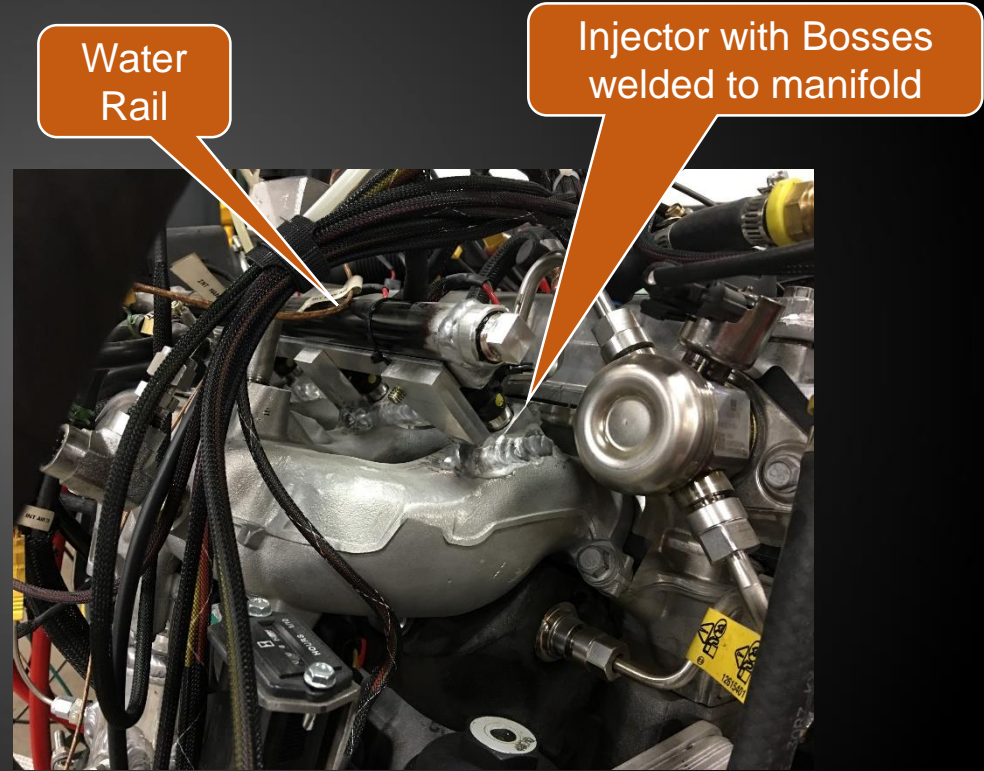
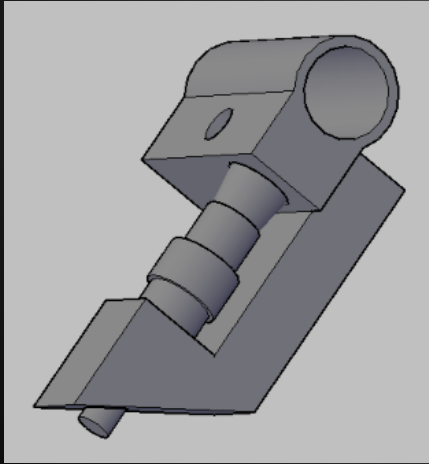
- SIDI 2.0L GM Ecotec LTG
- Twin Scroll Turbocharger
- Dual Independent Cam Phasing
- Large Aftermarket Support

Engine Specifications		
Base Engine	Displacement	2.0L
	Bore	86.0 mm
	Stroke	86.0 mm
	CR	9.2:1
Instrumentation	Dynamometer	350 kW AC
	Combustion	A&D CAS, AVL GH15D Pressure Transducers, BEI Optical Encoder
	Flow	Laminar Flow Element for Air Coriolis Meter for Fuel Coriolis Meter for Water
	General	Gauge & Absolute Pressures, Type K Thermocouples, Electronic Data Acquisition



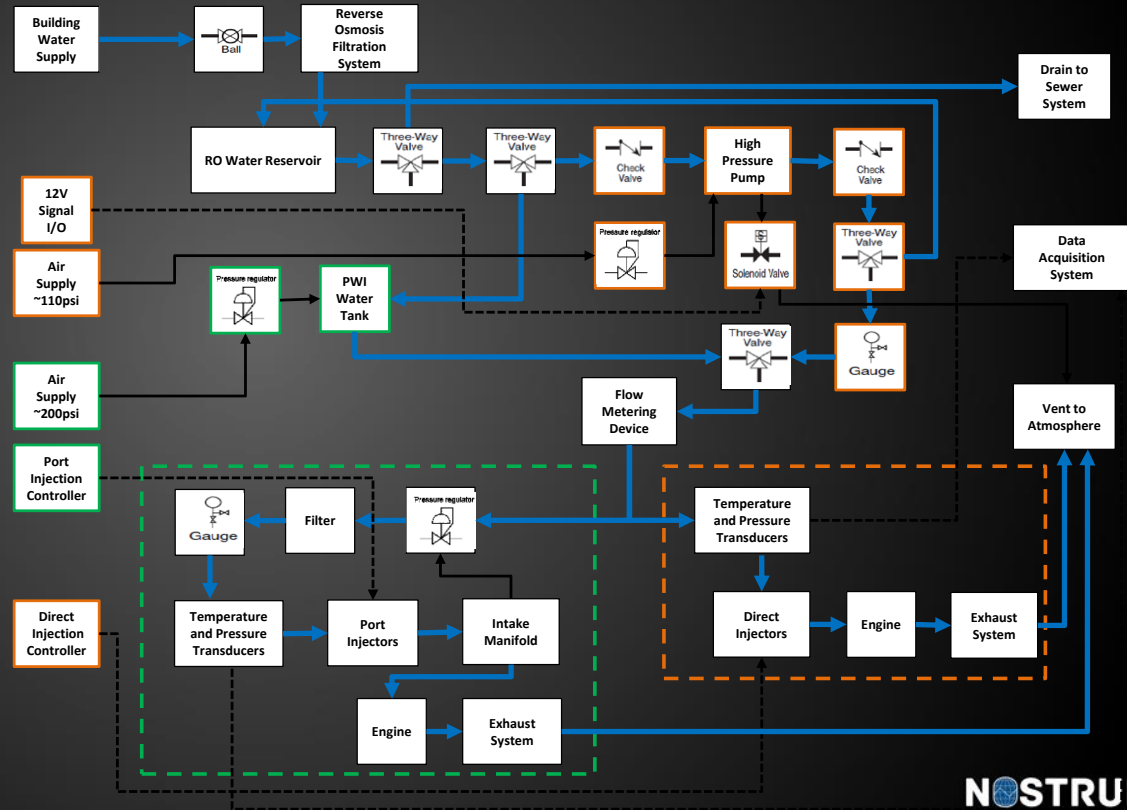
# Experimental Setup – Water Injection

- Injectors installed in intake manifold
- Direct Injection also an option



# Experimental Setup – Water Injection

- Test water is generated through Reverse Osmosis
- High Pressure supply (250 bar) for Direct Injection testing
- Low Pressure supply (10 bar) for Port Injection testing
- Flow measured with Coriolis meter



# Experimental Tests To Be Discussed

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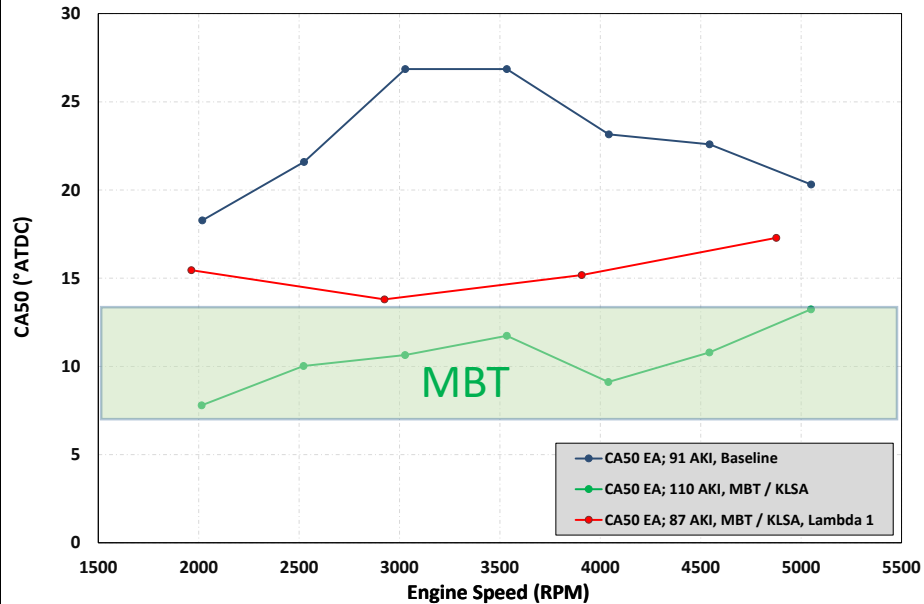
Test Number	Fuel	Water Injection	Spark Timing / Combustion Phasing	I-Cam	E-Cam	Lambda
Test 1	91 AKI (Engine manufacturer req.)	None	Production	Production	Production	Production
Test 2	110 AKI	None	10° CA50 or KLSA*	Production	Production	Production
Test 3	87 AKI	Port Injection	10° CA50 or KLSA*	Production	Production	1.0



# Experimental Results: Combustion

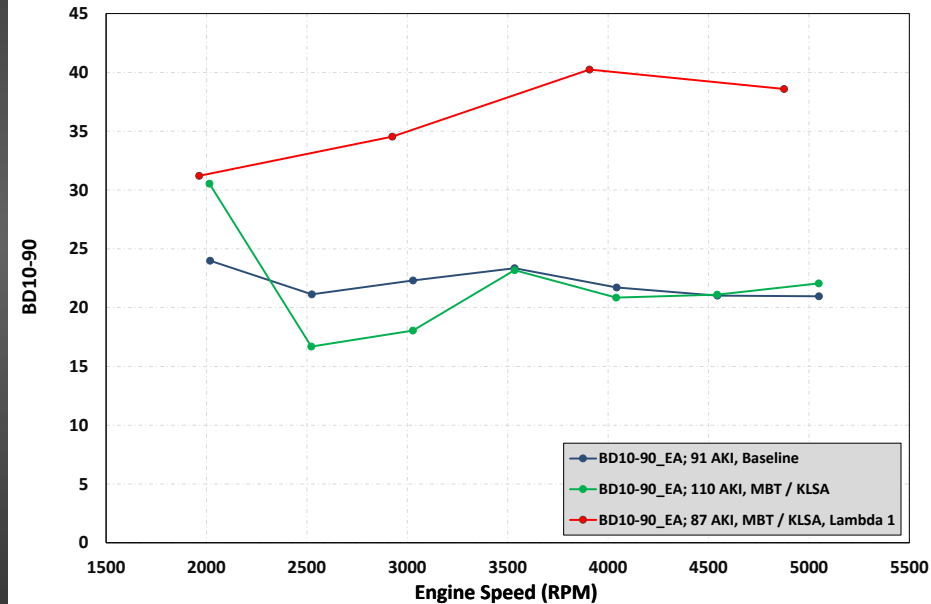
## Combustion Phasing

Baseline Engine

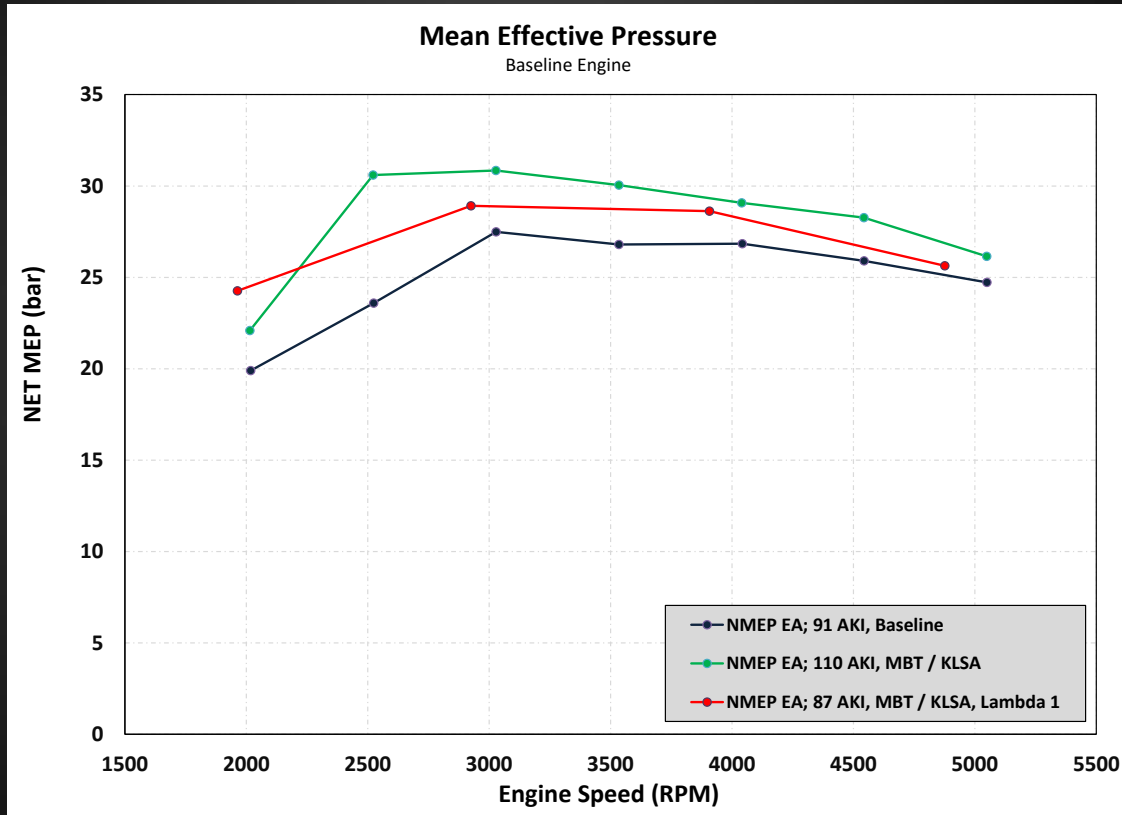


## Burn Duration

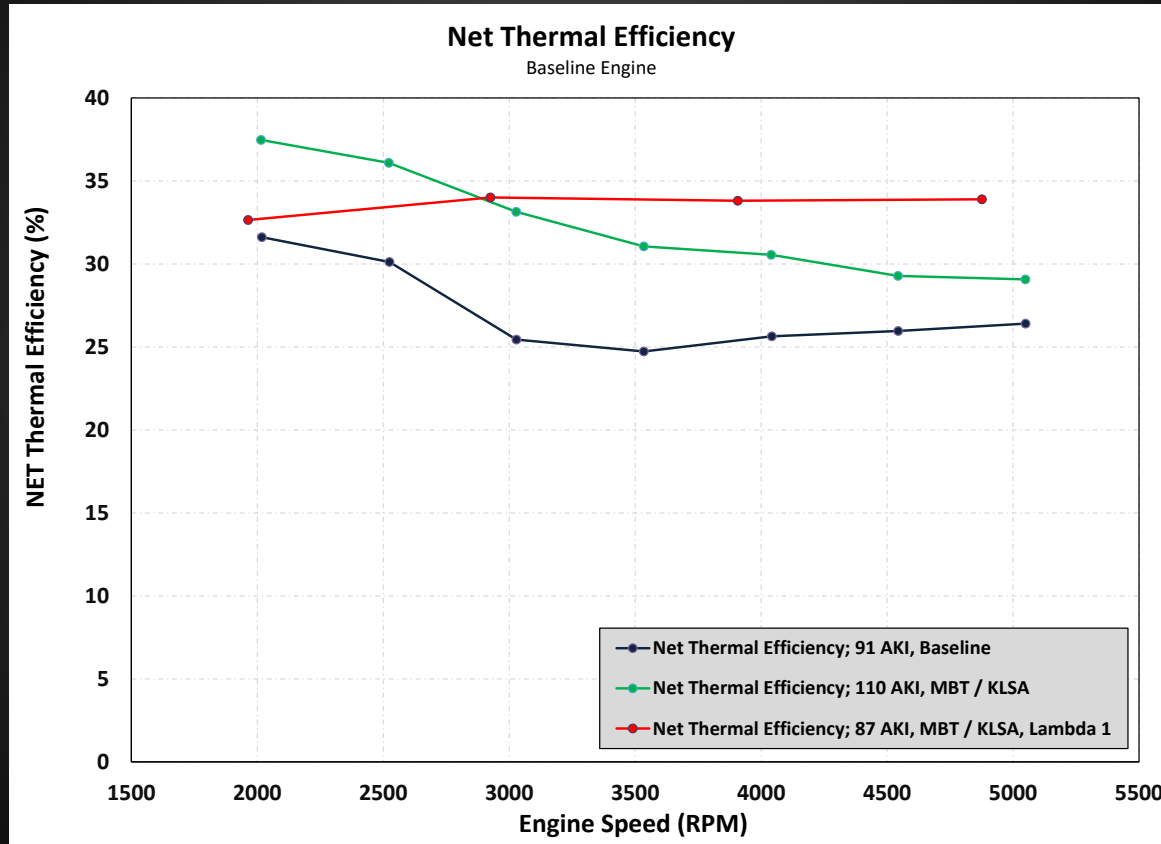
Baseline Engine



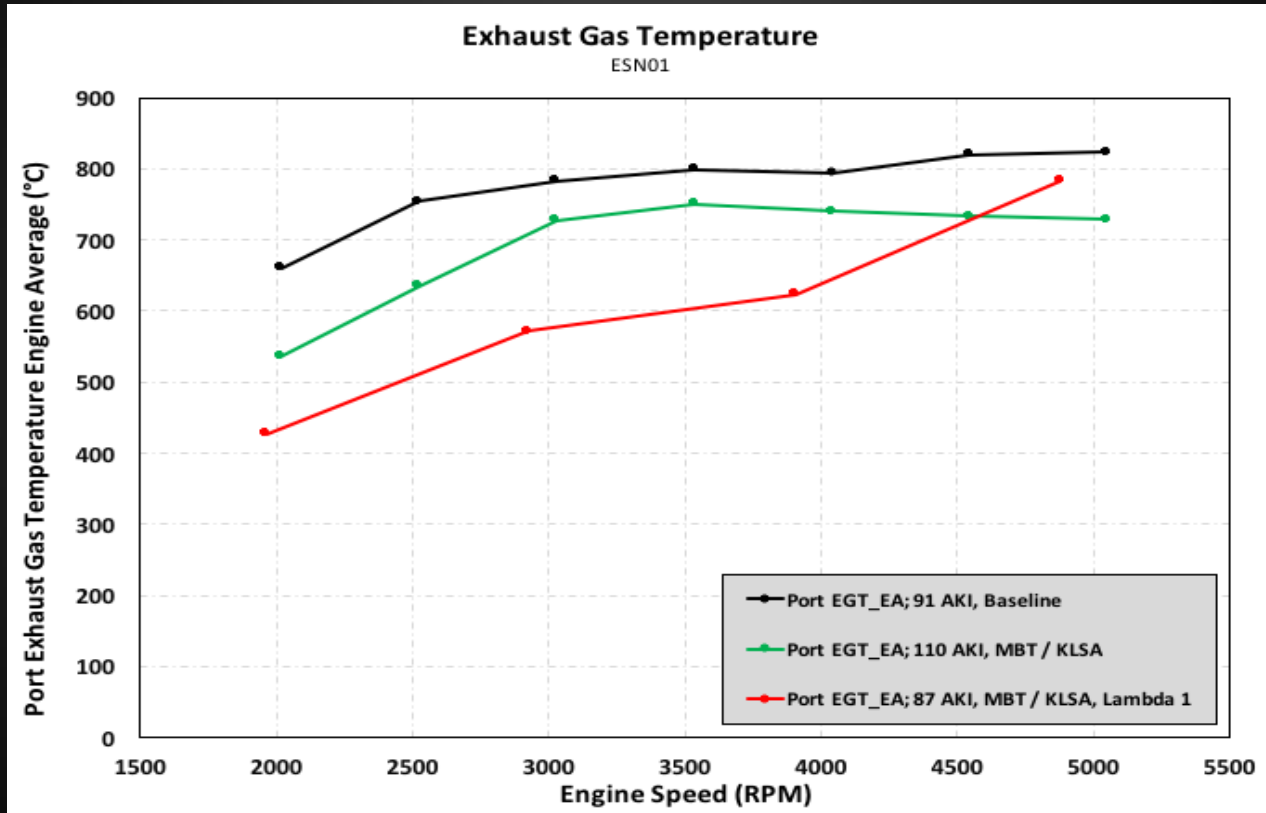
# Experimental Results; Output



# Experimental Results; Efficiency



# Experimental Results: Exhaust Gas Temperatures



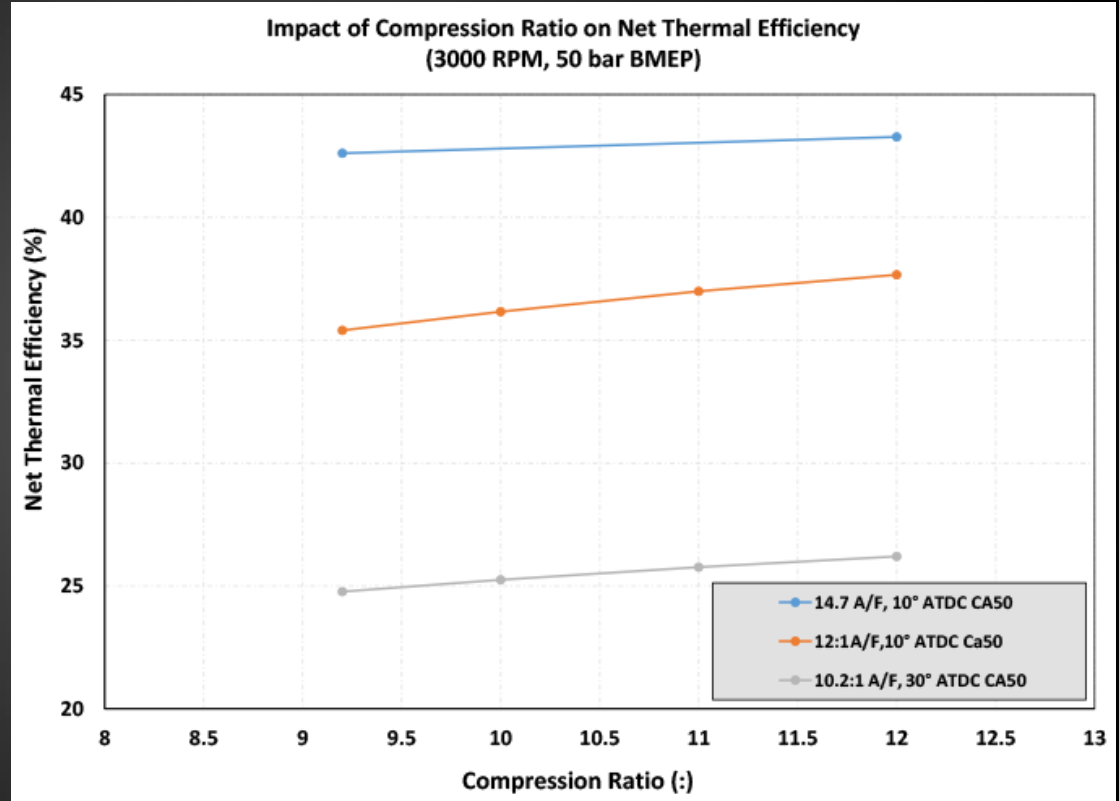
# Simulation

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- 1D Engine Simulation was utilized to scope the High BMEP Build (Target 50 bar BMEP)
  - Determination of required air pressure and flow
  - Investigation of peak cylinder pressure over a range of compression ratios
  - The same simulation model will be used to evaluate the impact of water injection

# Simulation Results

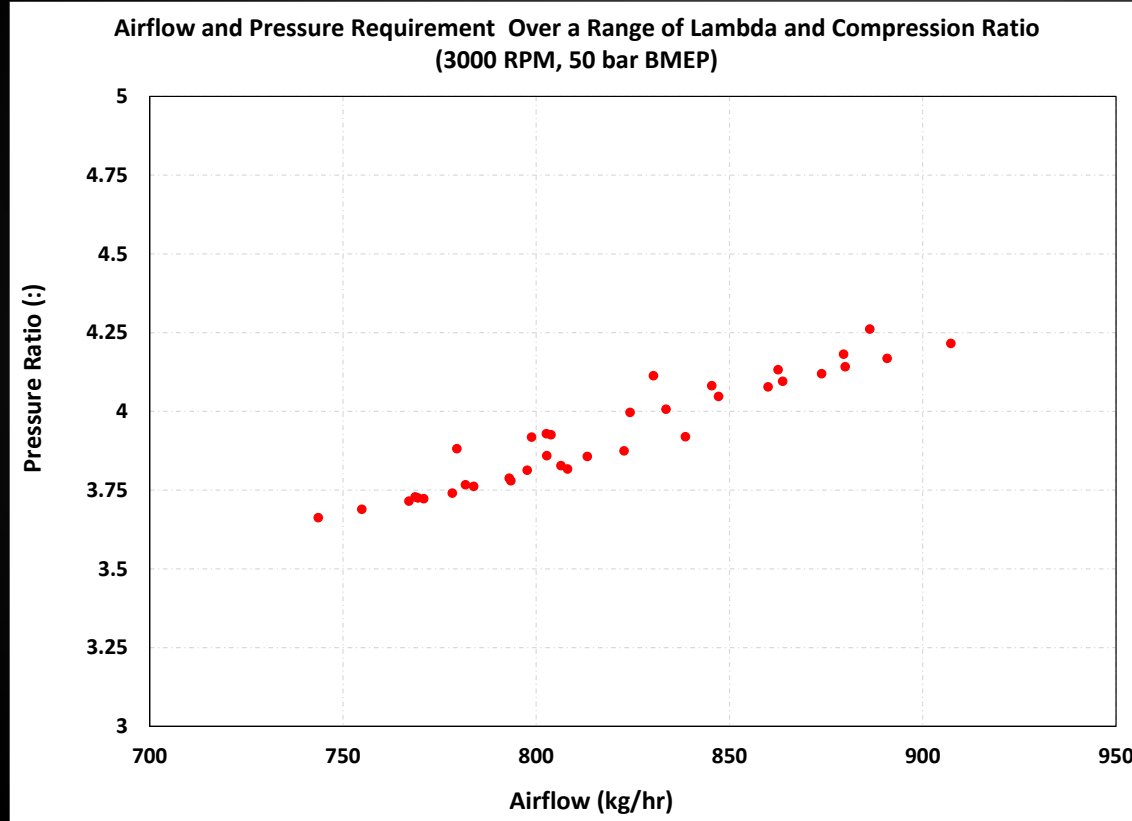
- Fuel Enrichment and Combustion Phasing both have large impact on Net Thermal Efficiency
- Good opportunity for efficiency improvements





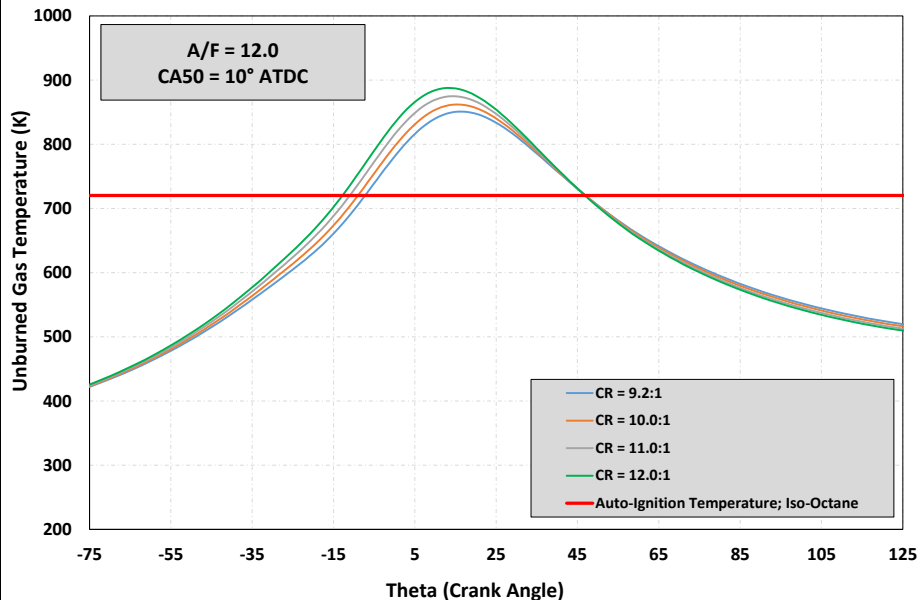
# Simulation Results

- Required P/R and mass flow are challenging for a single compressor
- Boost pressure is currently supplied via an external compressor
- Good candidate for alternative boosting systems (multi-stage, compounded)

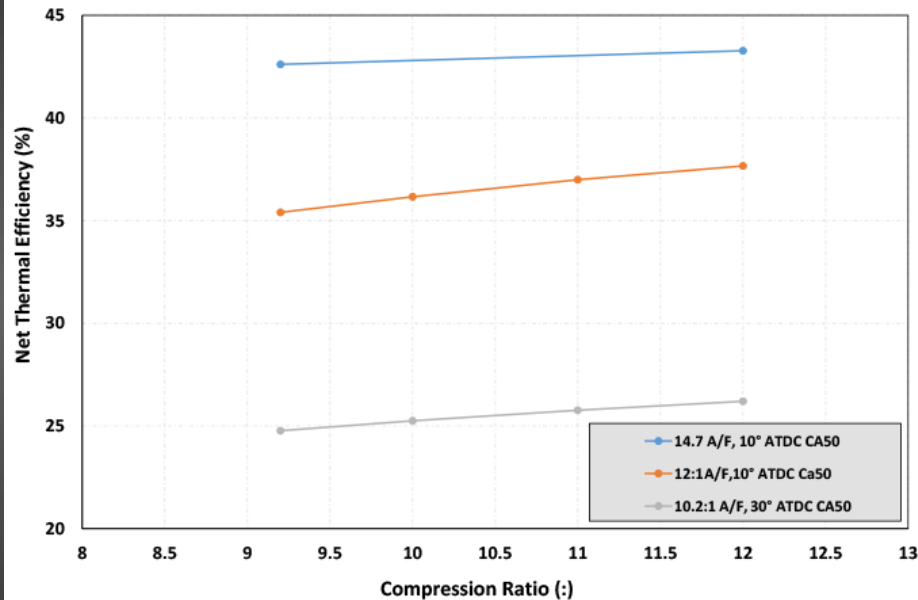


# Simulation Results

Impact of Compression Ratio on Unburned Gas Temperature  
(3000 RPM, 50 bar BMEP)



Impact of Compression Ratio on Net Thermal Efficiency  
(3000 RPM, 50 bar BMEP)



11.0:1 chosen as a compromise between efficiency, peak cylinder pressure, and unburned gas temperature (knock propensity)

# Water Injectors

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- Patented jet-to-jet collision breakup mechanism
- Reduced spray penetration and improved liquid atomization allow faster water vaporization rates

# Water Injectors used on this project

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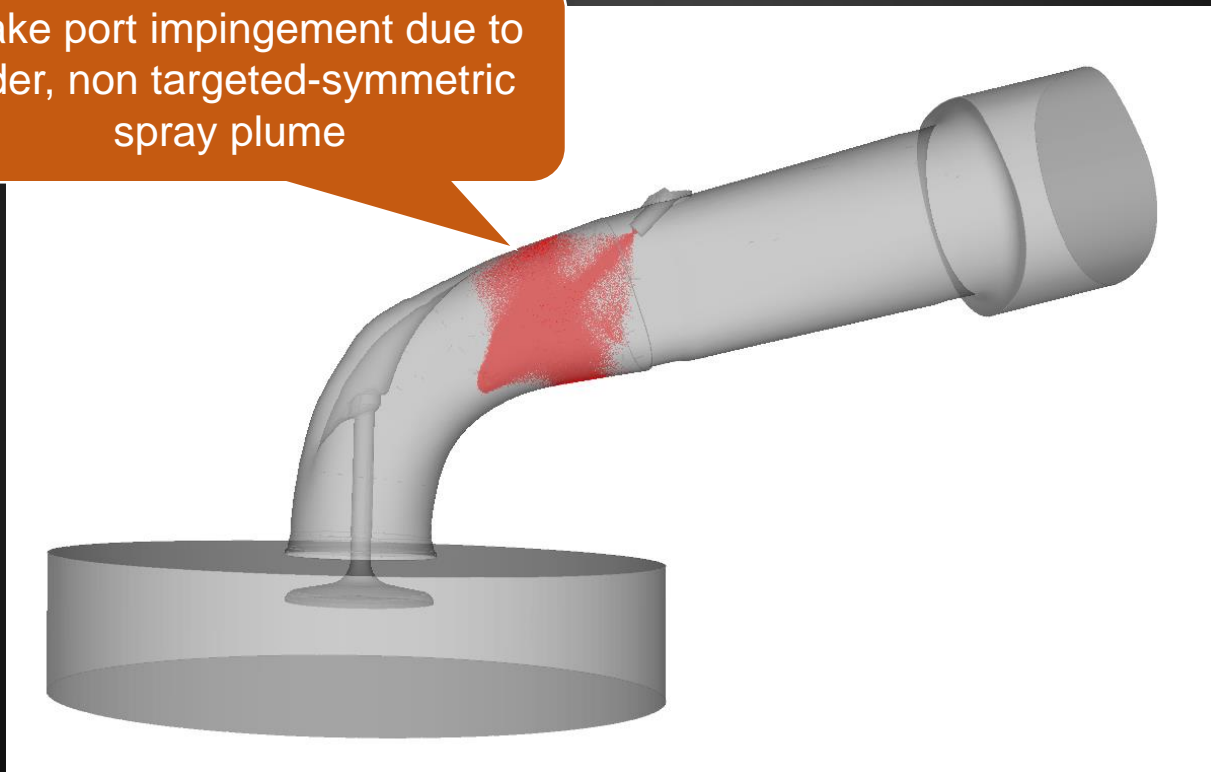
- Spray Targeted Nostrum KiWi; Kinetic Water Injector



- Nostrum Water DI injector (next phase)

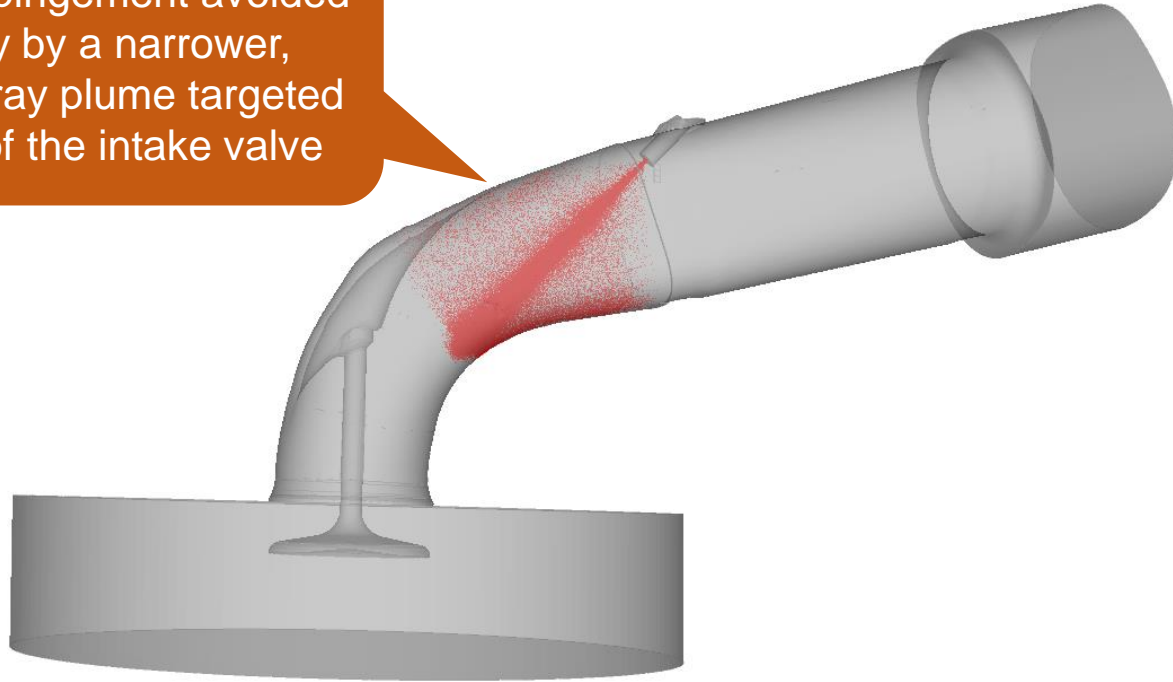
# PFI Spray Targeting – Symmetric Spray

Intake port impingement due to wider, non targeted-symmetric spray plume



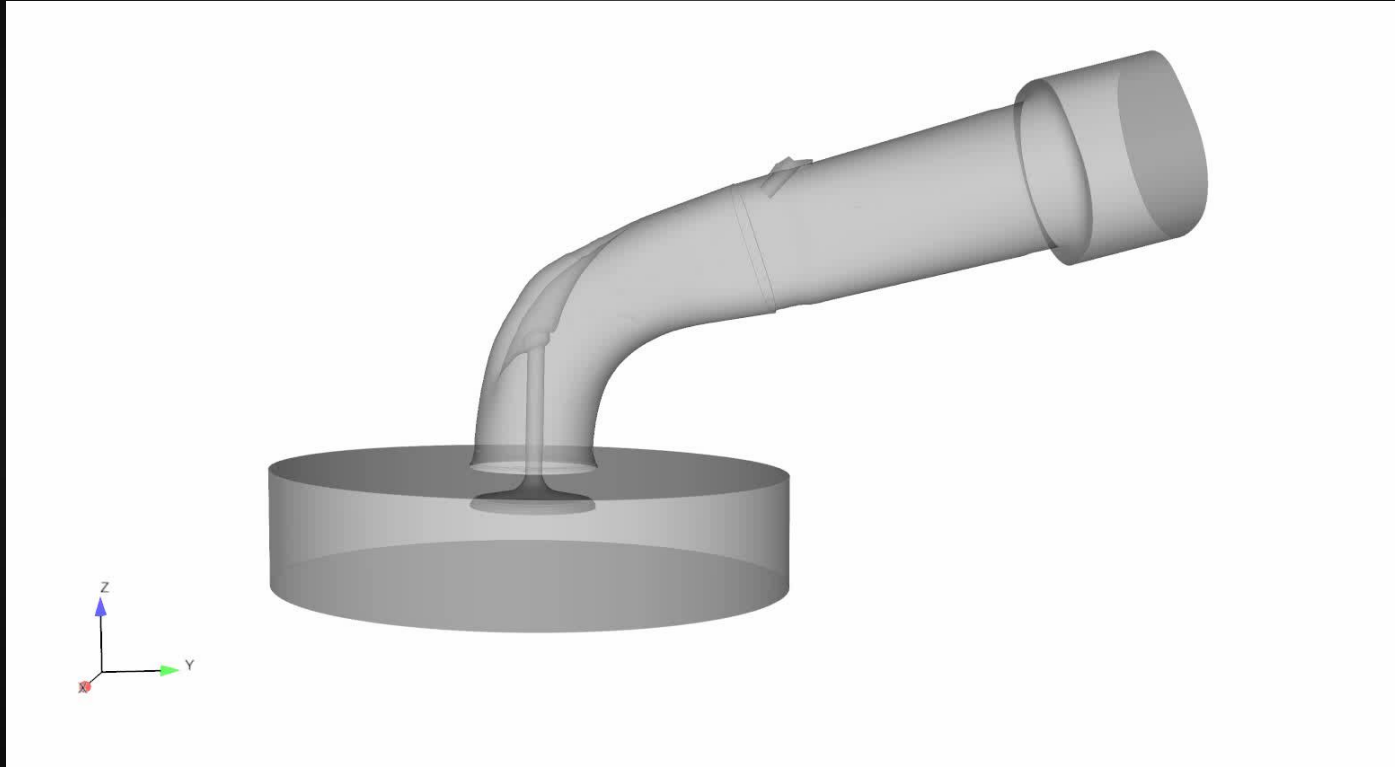
# PFI Spray Targeting – Directional Spray

Intake port impingement avoided significantly by a narrower, directional spray plume targeted to the back of the intake valve

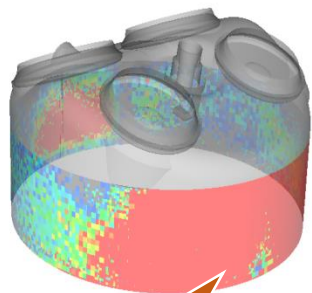




# PFI Spray Targeting – Directional Spray Movie



# Liner & Piston Impingement

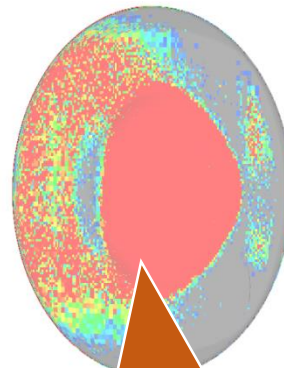


Crank\_angle = 676.01

film\_ht

1.000e-07  
9.526e-08  
9.053e-08  
8.579e-08  
8.105e-08  
7.632e-08  
7.158e-08  
6.684e-08  
6.211e-08  
5.737e-08  
5.263e-08  
4.789e-08  
4.316e-08  
3.842e-08  
3.368e-08  
2.895e-08  
2.421e-08  
1.947e-08  
1.474e-08  
1.000e-08

Fuel impingement on the liner due to improper spray targeting



Crank\_angle = 676.01

film\_ht

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9.526e-08  
9.053e-08  
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1.000e-08

Piston Impingement film

# Conclusions

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- Port water injection has been successfully demonstrated near current production best in class full load levels (~27 bar BMEP)
  - Enabled ***near MBT Combustion Phasing*** (water flow limited by instrumentation) on “Regular” 87 AKI Fuel and ***stoichiometric operation***
  - Resulted in a significant increase in Net Thermal Efficiency over production across all speeds
    - 34% @ 3000 RPM
  - Resulted in a significant increase in NMEP over production across all speeds

# Next Steps (Near Term)

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- Evaluate water injection at higher levels of BMEP
- Evaluate water injection at increased compression ratio
- Compare Direct Water Injection to Port Water Injection
- 1D Simulation of Water Injection
- Reduce water usage though spray targeting and reduction in droplet size

# High BMEP Engine Components

- Currently no production engine at this cylinder pressure
- Production intent
  - Forged Pistons & Connecting Rods
  - High Strength head studs
  - 10W40 High ZDDP Synthetic Oil
  - Increased valve lift
  - Increased valve spring stiffness
  - Larger High Pressure Fuel Pump
  - 83% increase in fuel flow



# Q&A

For full powerpoint



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